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# Block and boulder transport in Eastern Samar (Philippines) during Supertyphoon Haiyan

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## Abstract

Fields of dislocated boulders and blocks record catastrophic coastal flooding during strong storms or tsunamis and play a pivotal role in coastal hazard assessment. Along the rocky carbonate coast of Eastern Samar (Philippines) we documented longshore transport of a block of 180 t and boulders (up to 23.5 t) shifted uphill to elevations of up to 10 m above mean lower low water level during Supertyphoon Haiyan on 8 November 2013. Initiation-of-motion approaches indicate that boulder dislocation occurred with flow velocities of 6.3–8.3 ms<sup>-1</sup> which significantly exceeds depth-averaged flow velocities of a local coupled hydrodynamic and wave model (Delft3D) of the typhoon with a maximum < 1.5 ms<sup>-1</sup>. These results support the hypothesis that infragravity waves induced by the typhoon were responsible for the remarkable flooding pattern in E Samar, which are not resolved in phase-averaged storm surge models. Our findings show that tsunamis and hydrodynamic conditions induced by tropical cyclones may shift boulders of similar size and, therefore, demand to carefully reassess the possibility of storm-related transport where it, based on the boulder's sheer size, has previously been ascribed to tsunamis.

## 1 Introduction

Fields of dislocated boulders and blocks are among the most impressive sedimentary evidence of catastrophic coastal flooding (Williams and Hall, 2004; Scicchitano et al., 2007; Etienne et al., 2011; Goto et al., 2010, 2011; Nandasena et al., 2011; Richmond et al., 2011; Engel and May, 2012; Terry et al., 2013) and are widely used to infer the most extreme magnitudes of marine flooding events (tsunamis, storm surges) over large time scales (Etienne et al., 2011; Engel and May, 2012; Terry et al., 2013). Criteria to distinguish between tsunamis and storms include exponential landward fining of boulder fields or the generation of ridges due to strong storms, and more random scattering of boulders through tsunamis (Goto et al., 2010; Richmond et al., 2011). For

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some boulder deposits, storm transport was ruled out based on their large size, elevation and distance from the coast, and local extreme storm wave conditions (Scicchitano et al., 2007; Engel and May, 2012), while the long wave period of tsunamis has been associated with a higher transport competence (Lorang, 2011). However, the topic is still vividly debated (Goto et al., 2010; Lorang, 2011); until recently, only few studies provided unambiguous evidence for the transport of very large clasts during storms (Goto et al., 2011), e.g. based on direct observations, reliable historical documentation, or satellite data (Table 1). However, dimensions and transport distances of these clasts are often significantly smaller than those of palaeo-deposits for which the mode of transport is unknown.

We present evidence for onshore block and boulder dislocation at the carbonate coast of Eastern Samar (Philippines; Fig. 1) during Supertyphoon Haiyan (local name: Yolanda), one of the strongest tropical cyclones (TC) on record. Using sedimentary parameters of the clasts (spatial distribution, size, orientation, etc.), bi-temporal satellite images, characteristics of the storm surge and waves inferred from local numerical models, and inverse modelling of minimum flow velocities required to initiate boulder movement, we provide insights into the hydrodynamic and sedimentary processes during a TC. These insights have important implications for the boulder-related “storm vs. tsunami” debate.

## 2 Physical setting

Situated directly north of Leyte, the island of Samar is part of the Eastern Visayas (Philippines) (Fig. 1a). It is facing the Philippine Sea with the Philippine Trench and subduction zone to the east and the Philippine Fault to the west, the latter comprising a 1200 km long system of strike-slip faults crossing Leyte in a NW–SE direction (Barrier et al., 1991; Ramos and Tsutsumi, 2010). The inner part of Samar consists of Cretaceous to Oligocene igneous rocks, surrounded by mostly carbonate rocks of Mio-Pliocene age showing typical karst morphology (Traveglia et al., 1978).



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seconds (Mas et al., 2015); eyewitnesses on Leyte and Samar reported a threefold withdrawal of the sea followed by distinct flooding pulses. High flow velocities of up-rushing currents were inferred from a survivor video at Hernani, which approached for more than 1 min before receding (Gensis, 2013; Roeber and Bricker, 2015; Mas et al., 2015). Post-typhoon interviews with residents suggest that, similar to as TC Nargis had impacted Myanmar's Ayeyarwady delta in 2008 (Fritz et al., 2009), the coastal population of Leyte and E Samar lacked a proper understanding of the dimensions and devastating effects potentially connected with the term "storm surge". This lack of awareness is typically linked to the low frequency of such highest-magnitude events (Fritz et al., 2009), a relationship best described by inverse power-law functions (Corral et al., 2010). Personal experience and adaptation is commonly restricted to events of much smaller magnitude. This classical relationship emphasizes the pivotal role of geological records of extreme-wave events for coastal hazard assessment as they may provide information on local to regional frequency-magnitude patterns over millennial timescales and can also be implemented in education and raising awareness among residents (Weiss and Bourgeois, 2012).

The exposed coast of Eastern Samar is characterized by a large fetch and a steep offshore bathymetry. Hence, it experienced maximum wind speeds with the highest model-predicted waves of up to 19 m, but only a limited wind-driven surge during Haiyan (Bricker et al., 2014). Field indicators document inundation levels of up to 6 m onshore flow depth, nearly 11 m run-ups above local event tide level, and inundation distances of up to 800 m depending on onshore topography (Tajima et al., 2014; Shimozono et al., 2015).

### 3.3 Previous typhoons and storm systems

E Samar has repeatedly been impacted by severe typhoons in the historical past although they are generally less frequent compared to coastal areas further north. Catastrophic typhoons with tracks similar to the one of Haiyan occurred on 12–13 October 1897 (Soria et al., 2015), on 24–25 November 1912 (Philippine Weather Bu-

reau, 1912), and on 4 November 1984 (Typhoon Undang/Agnes, category 4 on SSSH) (JTWC, 1985). However, on historical time scales, Supertyphoon Haiyan is supposed to be the strongest typhoon to have hit E Samar (Lapidez et al., 2015).

Pre-Haiyan satellite images available for comparison with images captured after Haiyan date to 4 May 2013. Post-Haiyan images were captured three days after the typhoon on 11 November 2013, thereby excluding subsequent typhoons such as Basyang (31 January 2014; NDRRMC, 2014) for coarse-clast transport. Between 4 May 2013 and 8 November 2013, three storm systems occurred within an area of ca. 250 km N, S, and E of E Samar, according to the typhoon database of the Joint Typhoon Warning Center (JTWC, 2014). The tracks of two of these storm systems crossed an area of 120 km surrounding the study area, extending from the northern tip of Mindanao to northern Samar (Fig. 2). Tropical storm 30W (3 November–6 November 2013) only reached moderate wind speeds of  $\leq 60 \text{ km h}^{-1}$  when passing the 120 km radius, and its atmospheric pressure remained above 1000 hPa. Typhoon Rumbia (27 June–2 July 2013) had a northern track and made landfall at the City of Taft some 65 km north of the study area. However, it had maximum wind speeds of  $\leq 64 \text{ km h}^{-1}$  and reached a minimum atmospheric pressure of 996 hPa while approaching the coasts of E Samar and Leyte. Based on the low number of storm systems between May and November 2013 and their rather moderate intensity compared to Supertyphoon Haiyan, we ascribe any major block and boulder transport inferred from the satellite images to the latter event.

## 4 Methods and data

### 4.1 Interpretation of satellite images

Panchromatic satellite images of World View 1 (WV1, ID 1020010021141100, 4 May 2013) and WV2 (ID 10300100294524000, 11 November 2013) were used for mapping of the pre- and post-Haiyan position of wave-transported large clasts be-

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tween Hernani and the study site. The original georeferenced images were aligned based on unaltered coastal structures such as cliff edges using ESRI ArcGIS software, resulting in a positional accuracy of  $\sim 2$  pixel ( $\sim 1.2$  m). Satellite image-based mapping was restricted to clasts which were not covered/hidden by the dense vegetation on the pre-Haiyan image.

## 4.2 Field and laboratory work

In the field, the elevation of all dislocated clasts was measured using a Topcon HiPer Pro differential global positioning system (DGPS) with an altimetric accuracy of  $\pm 2$  cm. Elevations were referenced to mean lower low water level (MLLW). The first field survey was carried out in February 2014, three months after the typhoon. A second field survey was conducted between 5 and 20 March 2015. Altogether 59 clasts with longest axes  $> 1$  m were documented in the field at site ESA (Fig. 1b). The clasts were classified as “transported”, “not transported”, or “possibly transported” during Haiyan based on vegetation cover, weathering patterns and color of rock surfaces, the freshness of buried plant debris, and satellite imagery. Five of the dislocated boulders (ESA 1, 5, 7–9) were studied on high detail. The original (pre-transport) position of ESA 1 and 5 was identified based on fresh scars in the carbonate platform and the equal pattern of coral branches exposed within the scarp and at the clasts’ surface. The carbonate rock at the original position of ESA 7 and 9 appeared less weathered/karstified and has a significantly lighter color compared to surrounding platform sections, and a 5 cm high pedestal was documented at the pre-Haiyan position of ESA 9. The clasts’ trajectories and transport distances were identified by tracing impact marks on the carbonate platform using a DGPS. The distribution of fresh percussion marks on the clasts’ surface additionally gave evidence for their transport mode.

Two different approaches for calculating the clasts’ volumes ( $V$ ) were applied following the procedure described in a previous study (Engel and May, 2012): (i)  $a$  (length),  $b$  (width) and  $c$  (height) axes of the selected boulders were measured for conventional calculations of  $V_{abc} = a \cdot b \cdot c$  using a measuring tape. (ii) Upper and lower vertices and

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grass patches on top, a lack of impact marks at the surface, and a notch opening towards the base were documented for block ESA 9 and indicate sliding transport and no overturning.

Some 50 m to the north, numerous slab-shaped boulders were dislocated on top of the gently inclined Pleistocene carbonate platform. A boulder of  $\sim 23.5$  t (ESA 5:  $\sim 10$  m<sup>3</sup>;  $4.0 \times 2.8 \times 1.7$  m; Fig. 6a and b) was quarried at 2 m MLLW from the cliff edge of the carbonate platform leaving a fresh scarp, which was detected on the post-Haiyan satellite image as well (see also Sect. 5.1). It was transported vertically to 6 m MLLW by rolling or even saltation. Boulders of up to  $\sim 17$  t (e.g. ESA 1; Fig. 5d) were moved upwards from 6.5 to 10 m MLLW, 2 m below the highest run-up marks (Fig. 1c). Downward-facing rock pools and grass patches, still living barnacles, roots and soil staining on the exposed former bottom side, snapped palm trees, and fresh wood jammed under the rocks were found for the clasts on top of the Pleistocene carbonate platform as well (Fig. 6). The pre-Haiyan vegetation was almost entirely devastated, and flood debris display the limit of highest run-up at 12 m MLLW. The platform is covered by a thick sheet of whitish reef-borne sand and gravel overlying a brownish top soil horizon developed in an older carbonate sand deposit.

### 5.3 Calculation of flow velocities for block and boulder transport

Blocks and boulders may be moved by fluid forces in the form of sliding, rolling, or saltation (e.g., Nandasena et al., 2011), depending on flow velocity, bottom friction as well as the clasts' shape and weight. Based on the pioneering contributions of Nott (1997, 2003), Nandasena et al. (2011) presented improved hydrodynamic equations for calculating estimates of minimum flow velocities ( $u$ ) necessary for the initiation of coastal block and boulder motion by tsunamis and storms. The equation for the initial transport mode "sliding" of submerged or subaerial (e.g. ESA 9) clasts reads

$$u^2 \geq \frac{2 \cdot \left( \frac{\rho_s}{\rho_w} - 1 \right) \cdot g \cdot c \cdot (\mu_s \cdot \cos \theta + \sin \theta)}{C_d \cdot \frac{c}{b} + \mu_s \cdot C_l}, \quad (1)$$

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where  $\rho_s$  = density of the boulder =  $2.4 \text{ g cm}^{-3}$ ;  $\rho_w$  = density of sea water =  $1.02 \text{ g cm}^{-3}$ ;  $g$  = gravitational acceleration =  $9.81 \text{ ms}^{-2}$ ;  $c$  = boulder's shortest axis;  $b$  = boulder's second longest axis;  $\mu_s$  = coefficient of static friction = 0.7 (Nandasena et al., 2011);  $\theta$  = angle of the bed slope;  $C_d$  = coefficient of drag = 1.95;  $C_l$  = coefficient of lift = 0.178 (Nott, 1997; Noormets et al., 2004). The equation for the initial transport mode "rolling/overturning" of submerged or subaerial clasts (e.g. ESA 7) reads

$$u^2 \geq \frac{2 \cdot \left( \frac{\rho_s}{\rho_w} - 1 \right) \cdot g \cdot c \cdot \left( \cos \theta + \frac{c}{b} \cdot \sin \theta \right)}{C_d \cdot \frac{c^2}{b^2} + C_l}, \quad (2)$$

whereas the equation for the initial transport mode "saltation/lifting" of clasts in a joint-bounded scenario (e.g. ESA 5) is

$$u^2 \geq \frac{2 \cdot \left( \frac{\rho_s}{\rho_w} - 1 \right) \cdot g \cdot c \cdot \cos \theta}{C_l}. \quad (3)$$

Accordingly, boulder ESA 7 requires minimum flow velocities of  $5.2 \text{ ms}^{-1}$  to initiate sliding transport and of  $6.2 \text{ ms}^{-1}$  to initiate rolling transport. For the largest block ESA 9, initiation of sliding transport requires  $6.3 \text{ ms}^{-1}$ , and flow velocities of  $8.3 \text{ ms}^{-1}$  would have been required for overturning (Fig. 7).

On top of the carbonate platform, flow velocities of  $6.8 \text{ ms}^{-1}$  are necessary for the initial transport with overturning of ESA 1. For boulder ESA 5, which was quarried from the cliff edge (joint-bounded boulder scenario) and must have experienced saltation and lifting during initial transport, flow velocities were calculated to  $15.9 \text{ ms}^{-1}$ . The boulder transport histogram shown in Fig. 7 illustrates the critical flow velocities necessary for the initiation of different transport modes of each investigated clast.

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## 5.4 Storm surge and wave model

While previously published models resulted in maximum significant wave heights of 15 m during Haiyan in deep water off Eastern Samar (Bricker et al., 2014), maximum significant wave heights of  $\sim 4\text{--}5$  and  $\sim 5\text{--}6$  m are inferred for site ESA and for Hernani, respectively, from the here presented Delft3D model (Fig. 8a). This is comparable to maximum significant wave heights from recently published higher-resolution Delft3D models off the Holocene reef at Hernani (Roeber and Bricker, 2015).

Combining pressure- and wind-driven surge as well as wave setup, our coupled hydrodynamic and wave model results in slightly elevated maximum water levels ( $< 1$  m above mean sea level, a.s.l.), and maximum flow velocities below  $1.5\text{ m s}^{-1}$  (Fig. 8b and c) at site ESA during Haiyan. Flow velocities at Hernani and in Matarinao Bay reach highest values at 5:30 a.m. local time, while max. flow velocities at ESA are approached at  $\sim 8$  a.m. However, the modeled water levels are comparable to those inferred from previously published storm surge and FLO2D flood routing models (e.g., Bricker et al., 2014), where still water levels increase to a maximum of  $\sim 2.5$  m a.s.l. along the Hernani coast and in Matarinao Bay, but remain  $< 1$  m a.s.l. at site ESA.

Most recently, the high-resolution model of Roeber and Bricker (2015) resulted in surge-related maximum still water levels of 4 m a.s.l. at Hernani and maximum flow speeds of  $\sim 3\text{ m s}^{-1}$  off the reef crest; however, flow speeds still rapidly decrease to  $< 1.5\text{ m s}^{-1}$  on the reef platform and along the coastline, similar to the values presented here (Fig. 8b and c).

## 6 Discussion

### 6.1 Boulder transport and flow velocities inferred by inverse modelling

Based on field evidence, the interpretation of satellite images and the intensity of previous storms, the documented coarse-clast transport can unambiguously be attributed to

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marine flooding during Haiyan. The size of individual clasts and in particular the dimensions of block ESA 9 ( $9.0 \times 4.5 \times 3.5$  m), in combination with the documented vertical and lateral transport distances, exceeds any existing literature account including the often-cited boulder at Sydney's Bondi Beach (Süssmilch, 1912;  $6.1 \times 4.9 \times 3.0$  m), and clasts moved during TCs in Japan (Goto et al., 2011) and Jamaica (Khan et al., 2010) as well as during Atlantic winter storms (Williams and Hall, 2004; Regnaud et al., 2010; Cox et al., 2012) (Tables 1 and 2). According to the pedestal found at its pre-Haiyan position, block ESA 9 was stationary for a considerable period of time prior to Typhoon Haiyan (cf. Matsukura et al., 2007).

The largest transported clasts on the intertidal platform (ESA 7 and 9) show a shore-perpendicular orientation of their longest axis (Fig. 3). Their transport direction, as can be traced by impact marks on the carbonate platform and bitemporal satellite image analysis, coincides with the modeled flow vectors in direct vicinity of site ESA (Fig. 8) and, thus, with SE–NW-directed surge-accompanying water currents (Fig. 3). In contrast, for the rather flat boulders on top of the upper carbonate platform, the orientation of their longest axis is oblique to shore-parallel (Fig. 3), suggesting alignment to approaching superimposed storm waves and/or deflection of water currents on top of the reef platform by the  $\sim 2$  m high cliff.

However, flow velocities modelled with Delft3D are insufficient to account for the transport of the documented clasts (Fig. 8; see also Bricker et al., 2014; Roeber and Bricker, 2015). For boulder ESA 7, a rolling transport mode was inferred from the field observations requiring at least  $6.2 \text{ m s}^{-1}$  for the initiation of movement (Fig. 7) when assuming no vertical component in the transport track ( $\theta = 0.5$ ). In contrast, a sliding transport mode due to flow velocities higher than  $\sim 6.3 \text{ m s}^{-1}$  but below  $\sim 8.3 \text{ m s}^{-1}$  is assumed for dislocation of the largest block ESA 9 since no signs of overturning were observed. Consequently, flow speeds at this study site most probably exceeded  $6.3 \text{ m s}^{-1}$  but remained below  $8.3 \text{ m s}^{-1}$ . Calculated flow velocities for these clasts are thus in the range of or even higher than those inferred for recent major tsunamis at the coast (Fritz et al., 2006, 2012).

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Based on the applied formula, quarrying of ESA 5 from the cliff edge, as documented by the field survey, requires flow velocities of  $\sim 15.9 \text{ m s}^{-1}$  (Fig. 7). Since these flow velocities would have caused rolling transport of ESA 9, ambiguities remain for this joint-bounded scenario, which tends to derive significantly overestimated values (Switzer and Burston, 2010; Etienne, 2012). Discrepancies may for instance be related to the overestimation of strain forces between the block and the strongly karstified reef body, or to the underestimation of the waves' impact and lift forces approaching the cliffs and their associated jets (Hansom et al., 2008). However, flow velocities of  $7.1 \text{ m s}^{-1}$  are required for the subsequent rolling transport of ESA 5, which is in agreement with the flow velocities inferred from ESA 7 and 9. Against the background of previously published models and the modelled low flow velocities presented here, it is apparent that hydrodynamic processes have to be considered for the dislocation of the ESA clasts, which are beyond storm surge and incident waves.

## 6.2 Origin of exceptional flooding pattern

A very high velocity of the typhoon over the NW Pacific ( $32 \text{ km h}^{-1}$ ), an unusually warm subsurface ocean layer, and a long travel distance over the open ocean (3000 km) (Normile, 2013; Pun et al., 2013) probably provided the momentum for Haiyan's exceptional storm surge. For the Leyte Gulf and in particular San Pedro Bay off Tacloban, Mori et al. (2014) conclude that amplification of storm surge-induced water levels was due to seiches, also provoking the specific inundation pattern of distinct flooding pulses observed by residents.

In contrast, wind- and pressure-driven storm surge along the SE Samar coast is believed to not having exceeded  $\sim 1 \text{ m}$  due to the steep slope off the coast, but setup by breaking waves locally induced water levels of up to  $\sim 2.5 \text{ m}$  such as on top of the broad Holocene reef platforms (see also Bricker et al., 2014) or even 4 m at Hernani (Roerber and Bricker, 2015). However, in all phase-averaged (e.g., Delft3D/SWAN-based) coupled wave and storm surge models considering breaking-wave setup, including the here-presented one, modeled flow velocities on top and landward of the reef platform

remain  $< 1.5 \text{ ms}^{-1}$  (cf. Roeber and Bricker, 2015) and thus remarkably below those required for the clast transport documented at ESA during Haiyan.

To explain the surprisingly high inundation levels in SE Samar (Tajima et al., 2014) and the bore-like coastal flooding captured at Hernani (Mas et al., 2015), Bricker et al. (2014) hypothesized that infragravity waves (such as surf beat) (Munk, 1950) were caused by non-linear wave interactions with the reef, which are not resolved by the existing Delft3D and SWAN models. A Haiyan-related meteo-tsunami can be excluded due to a lack of bathymetric conditions with suitable resonance properties. Most recently, based on models simulating wave transformation over shallow fringing reefs using Boussinesq-type equations, Shimozono et al. (2015) and Roeber and Bricker (2015) confirmed that the extreme run-ups and the bore-like flooding pattern in E Samar must be explained by strong coupling of sea swells and infragravity waves with periods of several minutes, which may have experienced excitation by resonances with the fringing reef (Péquignet et al., 2009). These models inferred flow speeds of up to  $6 \text{ ms}^{-1}$  at the video site in Hernani, which is in good agreement with the flow speeds derived from (i) the video footage at Hernani (Roeber and Bricker, 2015); and (ii) initiation-of-motion criteria of the coarse-clast record presented in this study.

Surf beat resulting in pulses of elevated water depths and flow velocities is thus assumed as the driving process for the transport of the investigated boulders some 4 km north of the Hernani video site. However, regardless of the mechanisms responsible for the exceptional coastal flooding pattern, the sedimentary findings presented here give striking evidence of very high run-up and strong wave- and surge-accompanying sustained currents along the coast of SE Samar during Supertyphoon Haiyan. They were capable to transport block-sized clasts over horizontal distances of up to  $\sim 40 \text{ m}$  and to produce spatially randomized clast distributions, both which are often associated with tsunami deposition.

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## 7 Conclusions

Based on their SE–NW trajectory and a surge-perpendicular orientation of their longest axis (Fig. 3), we conclude that the exceptional flooding pattern, caused by wave setup and infragravity waves, induced the transport of the largest clasts rather than the high breaking waves alone. This is in contrast to many previous observations and descriptions of storm-moved boulders, which are defined to be “wave-transported” (Table 1). However, the shore-parallel orientation of the slab-shaped boulders on top of the carbonate platform may suggest that superimposed waves, having reached heights of more than 5 m (Bricker et al., 2014), contributed to their trajectory as well. The remarkable flooding pattern video-captured at Hernani thus affected a wider coastal section, i.e. ~ 5 km to the north, and was not restricted to special boundary conditions in urbanized areas such as sea wall structures at Hernani.

Supported by post-typhoon survey reports (Bricker et al., 2014; Tajima et al., 2014), recent wave models (Shimozono et al., 2015), eyewitness accounts and video footage (Mas et al., 2015; Roeber and Bricker, 2015), our findings suggest that a variety of hydrodynamic processes related to TC landfall must be considered when interpreting boulder deposits along coasts. The resulting sustained high-velocity coastal flooding in combination with inundation depths of several metres is capable of transporting clasts similar to palaeo-deposits commonly related to tsunamis. This is in agreement with theory-based conclusions of Weiss (2012) that both tsunamis and storms may shift clasts of comparable sizes. Our conclusions have important implications for the interpretation of coastal block and boulder deposits and numerical simulations of their transport in similar settings. Where storms have previously been ruled out to be the cause of the dislocation and transport of very large clasts based on their dimensions, the geological legacy of Haiyan prompts the need for a careful reconsideration of possible storm-related transport.

*Author contributions.* S. M. May, D. Brill, M. Engel, M. Reyes and H. Brückner contributed to field and lab work. S. M. May, D. Brill, M. Engel, and H. Brückner designed the study and

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interpreted the data. Modelling was done by C. Cuadra, A. M. F. Lagmay, J. Santiago and J. K. Suarez. Finally, S. M. May, D. Brill and M. Engel wrote the manuscript.

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**Table 1.** Boulder axes, volume and weight of very large storm-transported clasts from literature documented by eyewitnesses or remote sensing. Uncorrected and tentatively corrected volumes ( $V_{abc}$ ,  $V_{corr}$ ) and weights ( $W_{abc}$ ,  $W_{corr}$ ) are given using a correction factor of 0.6 (0.8 for the rather cubic boulder at Bondi, Boyson, 2012; Google Earth/Digital Globe, 2014).  $T_l$  = lateral transport;  $T_v$  = vertical transport;  $\rho_b$  = bulk density. The displacement of the above indicated clasts occurred due to direct storm wave impact. For the block at Bondi Beach the original source gives a weight of “about 235 t” (Süssmilch, 1912, p. 155), whereas multiplication of axes and local rock density of ca.  $2.35 \text{ g cm}^{-3}$  (Süssmilch, 1912; Verhoef, 1993) reveals only 211 metric tons. Furthermore, questions about the reliability of the report on the storm wave transport in 1912 have been raised, citing pre-1912 photographs of the boulder in its present position (Cass, 2002; Scheffers et al., 2008).

Site	$\rho_b$ ( $\text{g cm}^{-3}$ )	$T_l$ (m)	$T_v$ (m)	Dimensions (m)			Volume ( $\text{m}^3$ )		Weight (t)		Remarks and sources
				a axis	b axis	c axis	$V_{abc}$	$V_{corr}$	$W_{abc}$	$W_{corr}$	
Bondi Beach, Sydney (Australia)	2.35	50	–	6.1	4.9	3.0	89.7	71.7	211	169	Wave-transported during storm in 1912 (Süssmilch, 2012); often cited as an example for largest coastal boulder dimensions observed to have been moved during a storm (Felton and Crook, 2003; Switzer and Burston, 2010; Terry et al., 2013); values of dimensions and $\rho_b$ were taken from the original source (Süssmilch, 1912); a correction factor of 0.8 derived from recent photography (Boyson, no date; Google Earth/Digital Globe, 2014) of the boulder was applied for calculation of $V_{corr}$
Kudaka Island (Japan)	2.01	29	–	7.2	5.8	1.4	< 63	37.2	127	74.4	Wave-transported onto the intertidal reef platform during typhoon 6123 in 1961 based on an eyewitness report (Goto et al., 2011)
Okinawa Island (Japan)	NA	3	–	5.0	5.0	2.5	NA	NA	94	56.4	Wave-transported; moved by waves of typhoon 9021 on a 15 m high cliff-top in 1990 based on direct observations (Goto et al., 2011)
Manchioneal (Jamaica)	2.05	2	–	NA	NA	NA	NA	36.2	NA	79.7	Uplifted 2 m on a 12 m high cliff and moved 55 m inland; dislocation was documented after Hurricane Dean 2007; given dimensions are reliable and derive from multi-view image measurement (Khan et al., 2010)
Funafuti Atoll (Tuvalu)	NA	NA	NA	7.0	NA	NA	NA	NA	NA	NA	Wave-transported; moved and incorporated into a newly created rampart of coral rubble at the edge of a reef flat during cyclone Bébé in 1972 (Maragos et al., 1973)
Inisheer, Aran Islands (Ireland)	2.60	NA	2	NA	NA	NA	NA	NA	84	50.4	Wave-transported; moved onto a 2 m high limestone platform during a storm in 1941; larger blocks are reported within the boulder ridges, but their dislocation by storms has not been witnessed (Williams and Hall, 2004)
Inishmaan, Aran Islands (Ireland)	2.60	Several metres	–	11.5	4.0	0.65	29.9	17.9	78	46.8	Wave-transported; tabular boulder moved several metres laterally on a 17 m high cliff top during a storm in 1991 (Cox et al., 2012) based on a local eyewitness; incorporated in a boulder ridge
Ushant Island, Brittany (France)	2.70	Several metres	–	4.0	3.4	1.7	23.1	13.9	62.4	37.5	Wave-transported; boulder rafted in the intertidal zone for several metres during a storm in 2008 based on a post-storm survey (Regnaud et al., 2010)

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**Table 2.** Boulder axes, volume and weight of most important clasts at site ESA, E Samar.  $T_l$  = lateral transport;  $T_v$  = vertical transport;  $\rho_b$  = bulk density.

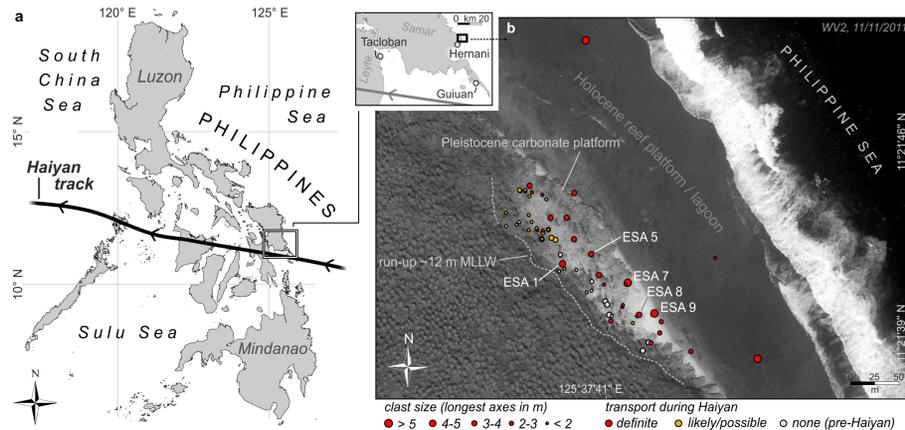
Boulder	$\rho_b$ ( $\text{gcm}^{-3}$ )	$T_l$ (m)	$T_v$ (m)	Dimensions (m)			Volume ( $\text{m}^3$ )		Weight (t)		$V_{\text{DGPS}}/$ $V_{\text{abc}}$	Remarks
				<i>a</i> axis	<i>b</i> axis	<i>c</i> axis	$V_{\text{abc}}$	$V_{\text{DGPS}}$	$W_{\text{abc}}$	$W_{\text{DGPS}}$		
ESA 1	2.4	20	2.5	4.6	2.3	1.1	11.6	6.9	27.9	16.7	0.60	Highest boulder, now resting at 10 m MLLW, vertical transport of 2.5 m, overturned
ESA 5	2.4	40	4	4.0	2.8	1.7	19.0	9.8	45.7	23.5	0.52	Vertical transport of 4 m, overturned, origin/fracture plain at 2 m MLLW
ESA 7	2.4	35	–	5.3	3.0	2.9	46.1	28.5	110.7	68.6	0.62	Upper littoral, lateral transport by rolling/saltation, overturned
ESA 8	2.4	> 40	> 2.5	3.6	2.70	1.80	17.5	9.1	42.0	21.8	0.52	Living barnacles and boring valves (former intertidal), overturned, assumed vertical transport of at least 2.5 m
ESA 9	2.4	45	–	9.00	4.50	3.50	121.5	75.3 <sup>a</sup>	291.6	180.8 <sup>a</sup>	(0.62) <sup>a</sup>	Largest block, upper intertidal, lateral transport by sliding

<sup>a</sup>  $V_{\text{abc}}$  of ESA 9 was corrected to  $V_{\text{DGPS}}$  using a conservative value of 0.6, which was empirically calculated for the similar-shaped boulder ESA 7.

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**Figure 1.** Study area and boulder field at site ESA. **(a)** Location of study area and Haiyan's track. **(b)** Setting of the boulder field at site ESA (59 clasts documented). The post-Haiyan image illustrates the extent of destroyed vegetation and deposited sand (light grey, on top of the Pleistocene carbonate platform) (WV2, 11 November 2013). Large clasts were moved on top of the Holocene reef as well as on top of the Pleistocene platform. A number of boulders (~30 clasts) were definitely transported, and dislocation of several further boulders is very likely. Further clasts must have been transported during an older palaeo-wave event.

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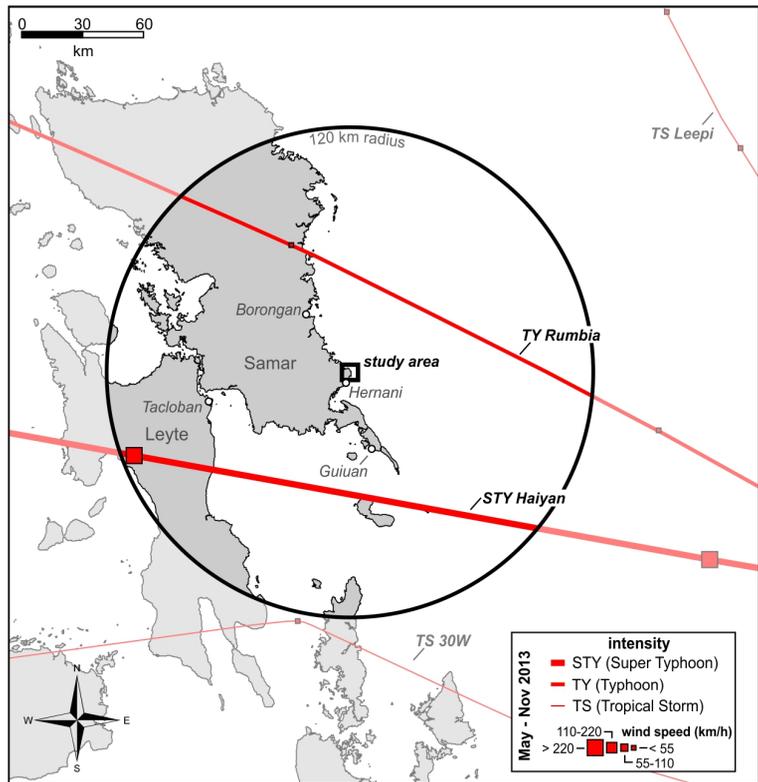
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**Figure 2.** Previous typhoons and tropical storms. Location of study area, track of Supertyphoon Haiyan, and tracks of three further storm systems which occurred within an area of ca. 250 km N, S, and E of E Samar between 4 May 2013 and 11 November 2013. (JTWC 2014). Tropical storm 30W (3 November–6 November 2013) and Typhoon Rumbia (27 June–2 July 2013) only reached moderate wind speeds of  $\leq 65 \text{ km h}^{-1}$  and atmospheric pressures of  $> 995 \text{ hPa}$  when passing the 120 km radius around the study area.

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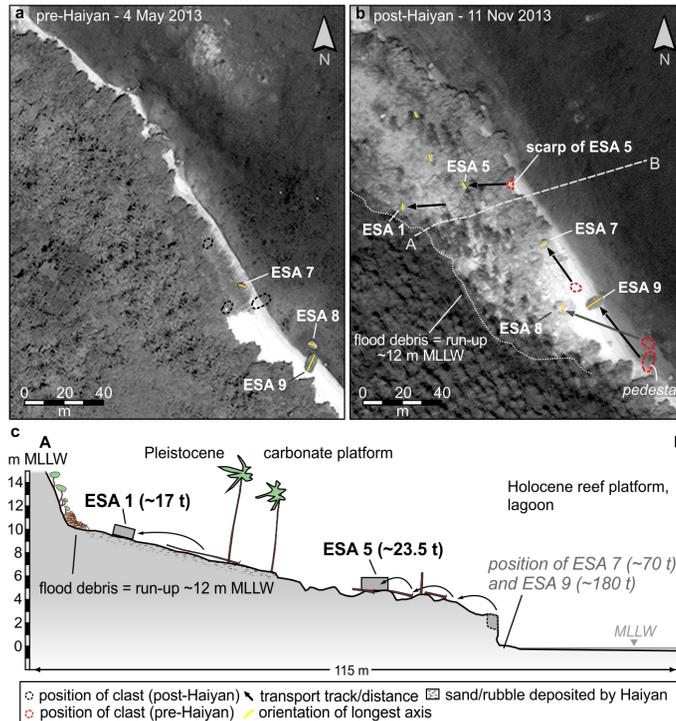
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**Figure 3.** Large clasts transported by Haiyan at site ESA. **(a, b)** Pre- (WV1, 4 May 2013) and post-Haiyan images (WV2, 11 November 2013) documenting run-up extent, position of clasts ESA 1, 5, 7, 8 and 9, and trajectories. Transport direction of largest clasts ESA 7 and 9 is SE–NW, coinciding with modeled flow vectors (Fig. 8) and, thus, with surge-accompanying water currents. ESA 9 was moved by  $\sim 40$  m. **(c)** Transect A–B. Flood debris at 12 m MLLW indicate maximum run-up. ESA 5: quarried from cliff edge.

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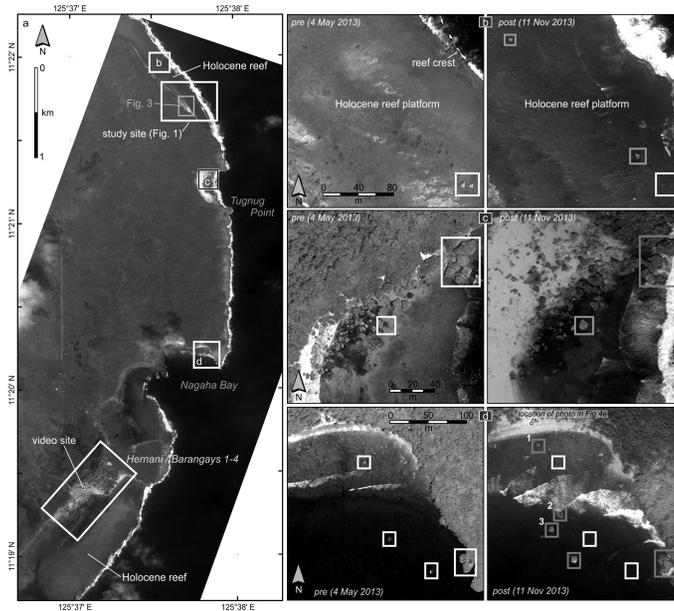
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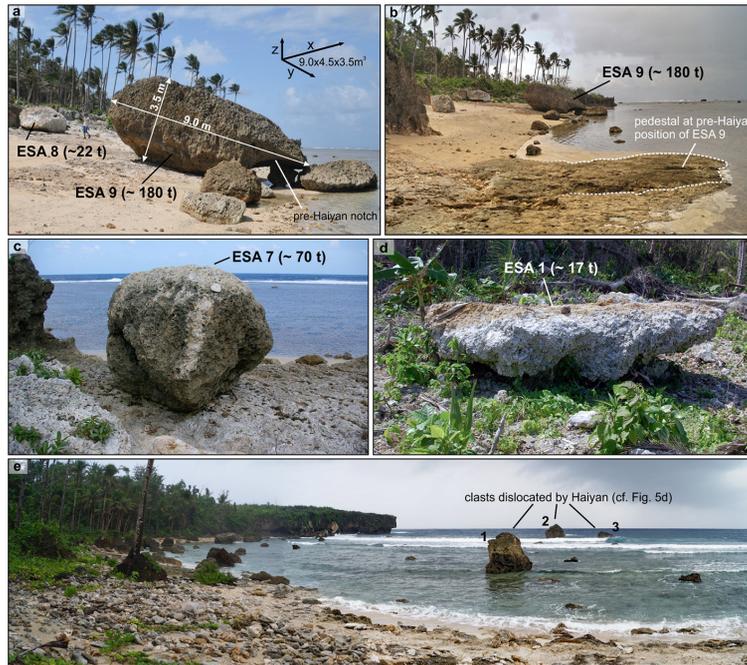
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**Figure 4.** Further evidence of block and boulder transport during Haiyan. **(a)** Location of study site ESA (see also Figs. 1 and 3), the City of Hernani including the location of the eyewitness footage (Gensis, 2013), and further sites **(b–d)** with evidence for Haiyan-induced block and boulder transport. **(b)** Two triangle-shaped blocks (with axis  $> 4$  and  $> 5$  m) were shifted on top of the Holocene reef platform, some 500 m north of site ESA; a distance of  $> 240$  m is inferred for the smaller one. **(c, d)** South of ESA numerous large clasts of pre-existing boulder fields changed position. Note dislocation (post-Haiyan imbrication) of large blocks (longest axis  $> 10$  m) directly west of the headland and of intertidal clasts to the west; clasts marked by 1–3 are shown in Fig. 5e **(d)**. White boxes mark pre-Haiyan positions, grey boxes post-Haiyan positions of clasts, or areas showing apparent movements of large clasts. Pre- and post-Haiyan satellite images are similar to Fig. 3.

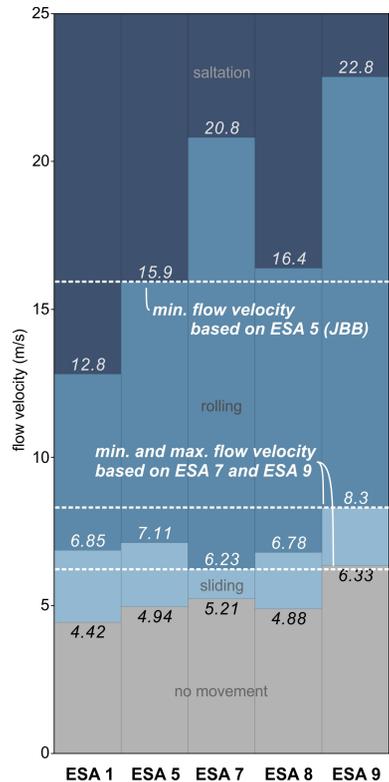


**Figure 5.** Photos of largest Haiyan-transported clasts at ESA. **(a)** Photo of ESA 9, the largest clast found at site ESA. **(b)** A ~ 5 cm high pedestal (foreground) was found at the pre-Haiyan position of ESA 9 (background). **(c)** Photo of ESA 7 looking from the SW towards the lagoon. **(d)** Boulder ESA 1, situated at ~ 10 m MLLW, directly below the run-up limit. **(e)** Panorama photo of Nagaha Bay (March 2015), view is to the SSE. Clasts 1–3 were dislocated by Haiyan, as documented by post-Haiyan satellite images (cf. Fig. 4d).

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**Figure 6.** Indicators of boulder movement during typhoon Haiyan. **(a)** Origin of boulder ESA 5, quarried from the cliff at ~ 2 m MLLW and transported upwards and landwards for 4 and 40 m, respectively. Snapped trees and impact marks on the carbonate platform can be traced on its trajectory. **(b)** Boulder at 6 m MLLW lying on top of freshly toppled palm trees. **(c)** Piece of wood jammed under boulder ESA 7. **(d)** Downward-facing and decaying grass patches at the former surface and new bottom side of ESA 7. **(e)** Percussion marks on the Pleistocene carbonate platform, tracing the transport track of ESA 5. Scale is 2 m. **(f)** Still living barnacle attached to boulder ESA 8, situated at 2.5 m MLLW, i.e. clearly above highest tide levels. **(g)** Roots and soil staining on the exposed former bottom side of several boulders (here boulder ESA 1) provide evidence of overturning during Haiyan.



**Figure 7.** Flow velocities calculated for transport of largest clasts at site ESA. For ESA 7, minimum flow velocities of  $6.23 \text{ m s}^{-1}$  were calculated using Eq. (2) to initiate rolling movement as observed in the field, which is similar to  $6.33 \text{ m s}^{-1}$  required to shift ESA 9. Since no signs for overturning were documented for ESA 9, flow velocities are assumed to have remained below  $8.3 \text{ m s}^{-1}$  based on using Eq. (1). However, based on the Eq. (3) of Nandasena et al. (2011), quarrying of ESA 5 required flow velocities of  $> 15 \text{ m s}^{-1}$ . JBB – joint-bounded boulder.

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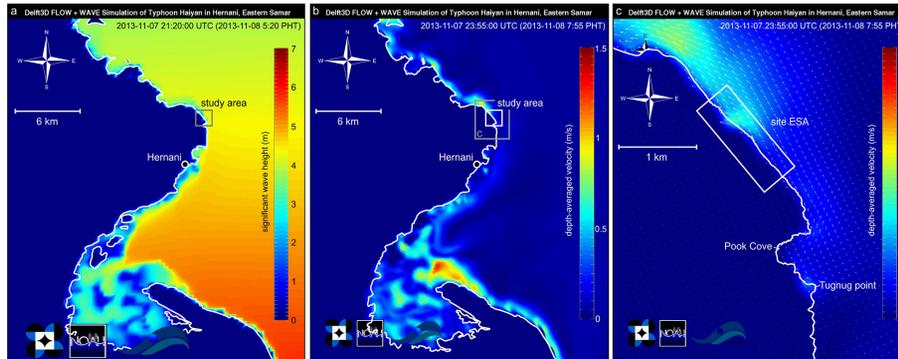
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**Figure 8.** Results from the (phase-averaged) wave and storm surge model using Delft3D and Delft Dashboard software. **(a)** Maximum significant wave heights in E Samar. In the study area, max. significant waves heights reached ca. 4–5 m at ~ 5 : 20 a.m. PHT. **(b, c)** Even in the coupled hydrodynamic and wave model, combining pressure- and wind-driven surge as well as wave setup, the max. depth-averaged flow velocities calculated for E Samar **(b)** and the study area **(c)** remain below  $1.5 \text{ m s}^{-1}$ . Highest velocities at ESA are approached at ~ 8 : 00 a.m. PHT. PHT – Philippines Time; UTC – Coordinated Universal Time.

